

**Practical Examples of First-Order ODEs.**

## POPULATION MODELS.

The basic model:  $n'(t) = rn(t)$ ,  $n$  is current population (not necessarily humans!),  $r$  is the *growth rate*; the particular form of  $r$  determines the particular model:

- (1) Elementary:  $r = B - M$ ,  $B$  is birth rate,  $M$  is mortality rate, both are constant; first suggested by a British economist Thomas Malthus (1766–1834) around 1800.
- (2) Logistic:  $r = B \left(1 - \frac{n}{\lambda}\right)$  (birth rate is constant but mortality rate is proportional to the current population); first suggested by Belgian mathematician P. F. Verhulst (1804–1849) around 1840 and allowed him to predict the US population 100 years later to within 1% error.
- (3) Logistic with threshold:  $r = -r_0 \left(1 - \frac{n}{\lambda}\right) \left(1 - \frac{n}{\mu}\right)$ .
- (4) Gompertz:  $r = r_0(\ln \lambda - \ln n)$ , first suggested by a British mathematician/actuary Benjamin Gompertz (1779–1865) around 1825.
- (5) Doomsday:  $r = r_0 n^\gamma$ ,  $0 < \gamma < 1$ . Proposed by H. von Foerster, P. M. Mora, and L. W. Amiot in the paper *Doomsday: Friday, 13 November, A.D. 2026*, Science 132 (November 1960): 1291–1295.
- (6) Nurgaliev:  $r = bn - M$  (now, mortality is constant but the birth rate is proportional to the current population).

CAPSTAN EQUATION (Euler 1769, Eytelwein 1808; Johann Albert Eytelwein (1764–1849) was a German civil engineer.)

A rope is winding around a capstan (a pole). Then

$$T_L = T_H e^{\mu\varphi},$$

where  $T_L$  is the load,  $T_H$  is the force needed to balance the load at the other end,  $\mu$  is the (dimensionless) coefficient of static friction between the rope and the surface [typically between 0.2 and 0.8], and  $\varphi$  is the winding angle (in radians). **With five complete turns ( $\varphi = 10\pi$ ) and  $\mu = 0.6$ , two pounds will balance an aircraft carrier.**

The reason: infinitesimal balance of forces,  $T$  (tension),  $N$  (normal reaction) and  $\mu N$  (friction) at the point of rope-pole contact. In the normal direction to the surface of the pole,  $\Delta N \approx T \Delta\varphi$ ; in the tangential direction (along the rope),  $\mu \Delta N \approx \Delta T$ . After eliminating  $N$ , get  $\Delta T \approx \mu T \Delta\varphi$  or, as a differential equation for  $T = T(\varphi)$ ,

$$T'(\varphi) = \mu T(\varphi), \quad T(0) = T_H.$$

NEWTON'S LAW OF COOLING. If  $T(t)$ ,  $t \geq 0$ , is the temperature of the object at time  $t$  and  $T_o < T(0)$  is the temperature of the environment, then

$$T'(t) = -\kappa(T(t) - T_o)$$

for some  $\kappa > 0$ .

GENERAL PROBLEM ON THE RATE OF CHANGE: “rate of change” = “rate in” – “rate out”. Two standard examples: mixing and loan payment.

MIXING. Assume that IN a container comes something (call it “pollutant”) as a perfect mixture at a (constant) rate  $a$  [volume/time] and with (constant) concentration  $\rho$  [mass/volume], and OUT of the container comes a perfect mixture at a (constant) rate  $b$  [volume/time]. Then the mass  $m = m(t)$  of the “pollutant” at time  $t$  satisfies

$$m'(t) = \rho a - \frac{m(t)}{V_0 + (a - b)t} b,$$

where  $V_0$  is the initial volume of the mixture in the container: the concentration of the pollutant in the container at time  $t$  is  $m(t)/V(t)$ , where  $V(t) = V_0 + (a - b)t$  is the current volume of the mixture in the container. If  $a \neq b$ , then the process will continue until either  $V_0 = (b - a)t$  (if  $b > a$  and the container becomes empty) or  $V_0 + (a - b)t = V_{max}$  (if  $a > b$  and the container is filled to capacity  $V_{max}$ ). If  $a = b$ , then

$$m'(t) = \rho a - \frac{m(t)}{V_0} a$$

and the process can continue for ever.

**LOAN PAYMENT.** If  $m$  is the amount you owe,  $r$  is interest rate (continuously compounded),  $T$  is the duration of the loan, and  $p$  is the payment rate (dollars per unit time), then, with “rate in” =  $rm(t)$ , “rate out” =  $p$ ,

$$m'(t) = rm(t) - p;$$

here the *terminal* condition  $m(T) = 0$ , together with the initial amount borrowed  $m(0)$ , determines the payment  $p$ .

**CATENARY:** the shape of a hanging cable. If  $y = y(x)$  is the shape,  $T_0$  is the horizontal tension at the lowest point  $(0, y_0)$ ,  $T$  is the tension at a point  $(x, y(x))$ ,  $m$  is the mass of the piece from  $(0, y_0)$  to  $(x, y(x))$ ,  $\rho$  is the mass of the cable **per unit length**,  $g$  is the gravitational constant, then

$$T \cos \theta = T_0 \quad (\text{horizontal balance of forces}); \quad T \sin \theta = mg \quad (\text{vertical balance of forces})$$

$$m = \rho \int_0^x \sqrt{1 + (y'(r))^2} dr \quad (\text{mass is density times arc length}),$$

and, keeping in mind that  $\tan \theta = y'(x)$ ,

$$y'(x) = \frac{\rho g}{T_0} \int_0^x \sqrt{1 + (y'(r))^2} dr.$$

Setting  $a = \rho g/T_0$  and  $u = y'$ , we get  $u' = a\sqrt{1 + u^2}$ , so that  $u(x) = \sinh(ax)$  and

$$y(x) = y_0 + \frac{1}{a} (\cosh(ax) - 1);$$

note that  $T_0$  has the units of force and therefore  $1/a = T_0/(\rho g)$  has the units of length, as it should.

### A separable ODE

$$f(y)y'(x) = g(x) \Rightarrow f(y)dy = g(x)dx \Rightarrow \int_{y_0}^y f(u)du = \int_{x_0}^x g(v)dv;$$

integrate, and solve for  $y$  (if possible).

*All of the above application examples lead to separable equations.* In particular, for some of the population models with  $t_0 = 0$ ,  $n(0) = n_0$ ,

$$n' = (B - M)n, \quad n(t) = n_0 e^{(B-M)t} \quad (\text{simple});$$

$$n' = B \left(1 - \frac{n}{\lambda}\right) n, \quad n(t) = \frac{\lambda n_0}{n_0 + (\lambda - n_0)e^{-Bt}} \quad (\text{logistic});$$

$$n' = r_0 (\ln \lambda - \ln n)n, \quad n(t) = \lambda \exp\left(\ln \frac{n_0}{\lambda} e^{-r_0 t}\right) \quad (\text{Gompertz});$$

$$n' = r_0 n^{1+\gamma}, \quad n(t) = \frac{\kappa^\kappa}{(\kappa n_0^\gamma - r_0 t)^\kappa}, \quad \kappa = \frac{1}{\gamma} \quad (\text{Doomsday}), \quad t_D = \frac{\kappa n_0^\gamma}{r_0}.$$